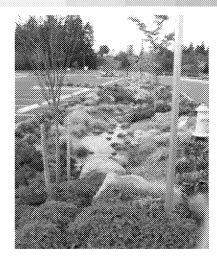


D & D ENGINEERING, INC.

Project Condor LOW IMPACT DEVELOPMENT (LID) REPORT

September 19, 2018

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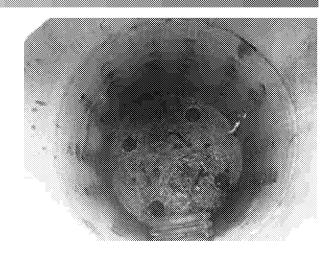






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I. Introduction

The purpose of this report is to outline and describe the proposed Low Impact Development (LID) strategies and Best Management Practices (BMPs) necessary to adequately reduce the hydrological and environmental impact of developing the proposed project, Project Condor, to comply with the requirements of LID Ordinance and LID Standard Manual¹. Additionally, this report will determine the storm water quality design volume (SWQDv) calculated from the 85th percentile, 24-hour rain event that is required to be treated. Finally, this report will also discuss the methodology used to arrive at these conclusions, the infrastructure necessary to support it and the operations and maintenance procedures required to maintain the system effective over time.

II. Project Description

Project Condor is comprised of three sites located near the intersection of Century Boulevard and Doty Avenue in the city of Inglewood. The first and main project site is located to the southwest of the intersection the second parcel is located to the southeast of the intersection, and the third piece is southwest of Century and Prairie intersection. The first site of the proposed development includes a multi-purpose sport arena, a parking structure and other miscellaneous use buildings. The site is located on an approximately 17-acre site bound by Century Blvd. on the North, Prairie Avenue on the West, Doty Avenue on the East and 103th Street on the South. The second site includes proposed surface parking over an approximately 5-acre parcel, not contiguous to the main project site, just east of Doty Avenue. The third site includes proposed surface parking over an approximately 5.5 acre parcel, not contiguous to the main project site, just west of Prairie Avenue north and south of existing W 101st street. to the project vicinity map, Figure 1 — Vicinity Map, for project site location.

Project Condor is a mixed-use project that includes a multi-purpose sport arena with auxiliary structures including retail, office buildings, restaurants, parking structures and plaza areas. The project consists of 71,000 sq. ft. of office space, 48,000 sq. ft. of retail and food service space, 85,000 sq. ft. of practice facilities, 25,000 sq. ft. of Sports Medicine Clinic. 15,000 sq. ft. of Community Space, an 18,000-fixed seat arena with an additional 500 temporary seats, a parking structure and substantial surface parking.

a. Existing Conditions

The existing site over the proposed main project site currently contains commercial buildings, a hotel, a fast-food restaurant and significant portions of vacant land. The existing site over the proposed surface parking site consists of five parcels that are currently all vacant. The existing site over the proposed surface parking west of Prairie Avenue site consists of thirty parcels that are currently all vacant.

Preliminary geotechnical investigations indicate that infiltration is infeasible for the site. The native soil characteristics are generally draining poorly and mostly heavily clayey or silty with an infiltration rate less than the LA County minimum for infiltration of 0.3 in/hr. Refer to the geotechnical report and recommendations, *Appendix A – Excerpt from Geotechnical Report*, for a summary of geotechnical findings.

b. Proposed Conditions

The proposed project seeks to develop the site into a mixed-use development composed of three general sites. The main site is considered the event area and includes a multi-purpose sports arena, retail/commercial buildings, a parking structure, and outdoor plaza. The east site proposes a parking structure, while the west site proposes surface

¹ (County of Los Angeles Department of Public Works, 2014)



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parking lots. Due to these improvements, it is estimated that approximately 90% of the project site will be covered by impervious surfaces.

III. Low Impact Development (LID) Stormwater Quality Control Measures

The Low Impact Development (LID) plan is intended to mitigate the hydrological and environmental stresses imposed on the site due to its proposed development. As the site's development typically increases impervious level, so does the stormwater runoff volume and the amount of environmental pollutant it produces. The goal of the LID plan is to mitigate these factors by both reducing the volume of stormwater and potential pollutants in stormwater runoff to the most reasonable extent possible. This strategy may be accomplished by implementing a variety of Best Management Practices (BMPs) stormwater quality control measures designed to handle the frequent, smaller storm event, or the initial volume of stormwater run-off from a larger storm event (referred as first flush). This study will focus on and follow the procedures for selecting and implementing stormwater quality measures, as recommended in the Los Angeles County Department of Public Works (LACDPW) Low Impact Development Standards Manual.

a. Los Angeles County Design Guidelines

The focus of the design criteria for stormwater control measures is the construction and implementation of stormwater quality control measures that meet stormwater runoff requirements in terms of on-site retention and pollutant removal. The project must design and implement stormwater quality control measures that can handle the SWQDv. Any surplus storm run-off must be diverted around the stormwater quality control measures to prevent overloading. The Los Angeles County Department of Public Works Low Impact Development Standards Manual categorized stormwater control quality measures into the following types listed in level of priority:

- 1. Retention based BMPs (bioretention, infiltration basin, drywells, capture and reuse cisterns, green roof)
- 2. Biofiltration BMPs (biofiltration)
- 3. Vegetation-based BMPs (stormwater planters, vegetated swales, tree-well filter, etc.)
- 4. Treatment-based BMPs (Extended detention basin, constructed wetlands, wet pond, sand filters, proprietary devices)

Systems in a lower priority level may only be used if higher priority measures are deemed to be technically infeasible as set forth in the county's standards manual. Due to the properties of the native soils and the tendency to percolate well, this study will focus on retention-based BMPs.

b. Proposed Low Impact Development (LID) System

The proposed Low Impact Development (LID) system will utilize a combination of county standard bio-filtration planters and proprietary bio-filtration systems by Contech to treat the SWQDv from the 85th percentile, 24-hour storm. This will be accomplished through directing runoff from drainage areas to onsite bio-filtration planters and bio-swales currently proposed as part of the site hydrology study.

The proposed bio-filtration systems are designed to capture site runoff from roof drains, treat the runoff through biological reactions within the planter soil media, and discharge at a rate intended to mimic pre-developed conditions. Refer to the specific system configurations, *Figure 3 – Site Specific Bio-Filtration Details*, for bio-filtration system configurations at their given locations. Sizing and capacity analysis of the proposed conventional bio-filtration systems will be calculated by following the design guidelines defined through the State of California Los Angeles Regional Water Quality Control Board. It is anticipated that the city of Inglewood will apply directly to the water board for approval. Once approval is granted to the city of Inglewood, only city approval is required for continuation. In addition, county approval of the proprietary Contech Bio-Scape Filterra systems will be pursued for this project. The system has been previously approved within the county for several other jurisdictions, this LID plan will seek to receive approval for Filterra systems specifically for use within the city for Inglewood.



IV. Hydromodification Analysis

As outlined in Section 8.2 of the Los Angeles County Department of Public Works Low Impact Development Standards Manual, projects may be exempt from implementation of hydromodification control measures where assessments of downstream channel conditions and proposed discharge hydrology indicate that adverse hydromodification effects to beneficial uses of natural drainage systems are unlikely. Since the proposed project site will discharge through a storm drain system into the concrete Dominguez Channel, the project is exempt from Hydromodification Control Measures.

V. Site Design BMPs

a. Site Design

Current water quality requirements are based on treating a specific volume of stormwater run-off from the project site (SWQDv). The design storm from which the SWQDv is calculated is defined as the greater of:

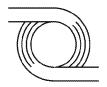
- ∞ The 0.75-inch, 24-hour rain event, or
- ∞ The 85th percentile, 24-hour rain event as determine by the Los Angeles County 85th percentile precipitation isohyetal map

The volume of stormwater run-off that must be retained at a project site is calculated using MODRAT. In this case, the SQWDv volume from the 85th percentile, 24-hour rain event will be utilized. LACDPW developed a hydrologic calculator (HydroCalc) that completes the full MODRAT calculation process and produce the SWQDv volumes and flow rates for single subareas. This report will utilize the results from HydroCalc as a means of determining the stormwater quality design volumes (SWQDv). The proposed site was divided into drainage sub-areas, based on the proposed site grading and proposed drainage patterns. Refer to the Conceptual Low Impact Development Exhibit, Figure 2 – Conceptual Low Impact Development (LID) Exhibit, for the definition of the drainage sub areas. The following table, Table 1 - Post-Development Conditions, summarizes the results of the study and required treating volumes SWQDv for each subarea.

TABLE 1 - POST-DEVELOPMENT CONDITIONS AND BMP SUFFICIENCY SUMMARY

Project Condor

Designation	Drain and		В	MP Sufficiency Su	mmary		
Drainage Subarea	Area (sf)	Q _{pm} (cfs)	SWQDv x 1.5 (cf)	Bio-Filtration System	Required (sf)	Provided (sf)	Sufficient
DA-1	90,537	0.5852	9,671	Planter - Type B	3,868	4,605	Yes
DA-2	33,854	0.304	3,627	Planter – Type B	1,451	2,332	Yes
DA-3	43,992	0.3936	4,697	Planter – Type B	1,879	3,032	Yes
DA-4	12,631	0.0889	1,349	Filterra	43	48	Yes
DA-5	71,114	0.5549	7,578	Filterra	256	307	Yes
DA-6	16,104	0.11	1,721	Filterra	55	60	Yes
DA-7	23,742	0.1302	2,558	Filterra	73	91	Yes
DA-8	89,119	0.4537	9,531	Filterra	264	273	Yes
DA-9	25,185	0.1398	2,697	Filterra	78	91	Yes
DA-10	46,835	0.331	5,022	Filterra	160	182	Yes



Totals	1,101,446	7.8659	120,855				
RDA-6C	80,006	0.5915	8,972	Planter – Type A	3,589	3,589	Yes
RDA-6B	39,726	0.3384	4,437	Planter – Type A	1,775	1,964	Yes
RDA-6A	79,803	0.5883	8,924	Planter – Type A	3,569	3,569	Yes
RDA-5	87,796	0.63	9,851	Planter – Type A	3,940	4,564	Yes
RDA-4B	155,867	1.0053	17,457	Planter – Type A	6,983	7,149	Yes
RDA-4A	155,572	0.9798	17407.5	Planter – Type B	6963	7324	Yes
RDA-3	5,595	0.0562	635	Planter – Type A	253.8	288	Yes
RDA-2	21,411	0.1906	2,390	Planter – Type A	955.8	1610	Yes
RDA-1	14,326	0.1518	1,610	Planter – Type A	643.8	692	Yes
						D	& D ENGINEERING,

^{*}Proposed proprietary Filterra bio-filtration system. See Appendix C for alternative design criteria calculations.

Refer to Appendix B – Site Design Calculations for each subarea HydroCalc worksheets.

Refer to Appendix C - Sizing Calculations for each Bio-Filtration System calculation.

b. BMP Selection

All roof drainage areas, as listed in the table above, discharge via roof drains to bio-filtration planters located on the surface. The remaining roof and drainage areas will be directed to a proprietary biofiltration system designed by Contech. Refer to the conceptual low Impact Development (LID) Exhibit, Figure 2 – Conceptual Low Impact Development (LID) Exhibit, for stormwater routing.

Refer to the calculation sheets in *Appendix C – Bio-Filtration Sizing Calculations*, for detailed calculations demonstrating the capacity of each proposed bio-filtration system.

VI. Summary and Conclusion

To summarize, the proposed low impact development (LID) system stormwater quality control measures and structural source measures are adequately designed and sized to accomplish the following:

- ∞ Capture and mitigate the SQWDv volume from the 85th percentile, 24-hour storm;
- ∞ Bio-filtration of captured volume by bio-filtration through a combination of standard bio-filtration planters and proprietary bio-filtration systems.
- Prevent pollutants from contacting stormwater run-off and/or prevent discharge of contaminated stormwater run-off to stormdrain system

Based on the calculations and conclusions presented in this report, the proposed LID stormwater quality control measures will retain on-site through bio-filtration and will mitigate the required SWQDv volumes as defined by the Los Angeles County Department of Public Works Low Impact Development Standards Manual.



VII. References

County of Los Angeles Department of Public Works. (2014). Low Impact Development Standards Manual. Los Angeles.

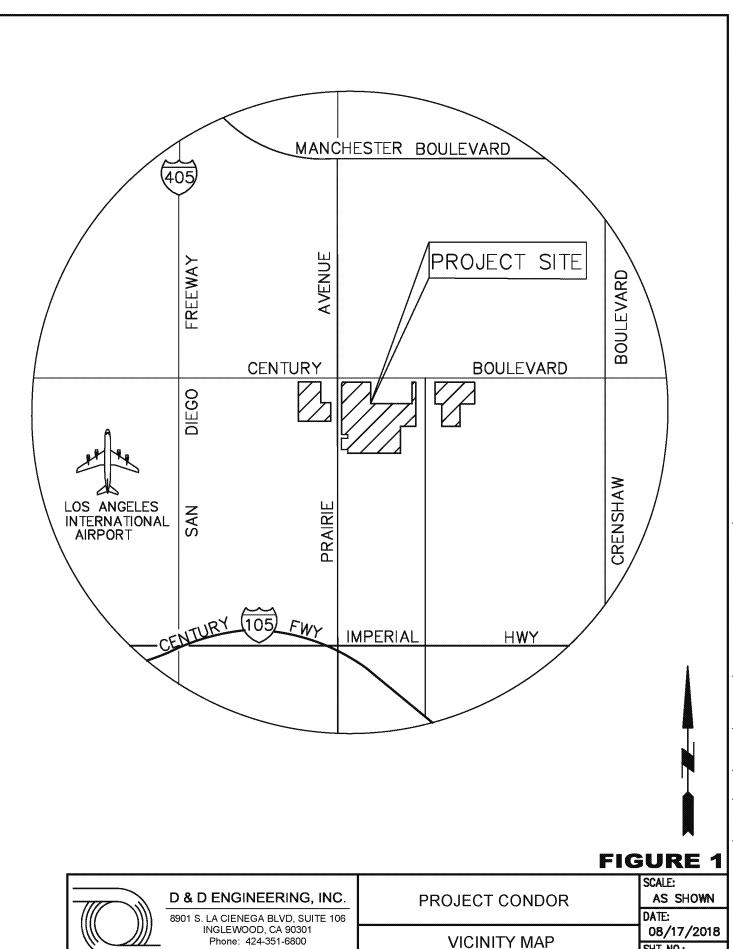


FIGURES

Figure 1 — Vicinity Map

Figure 2 — Conceptual Low Impact Development (LID)

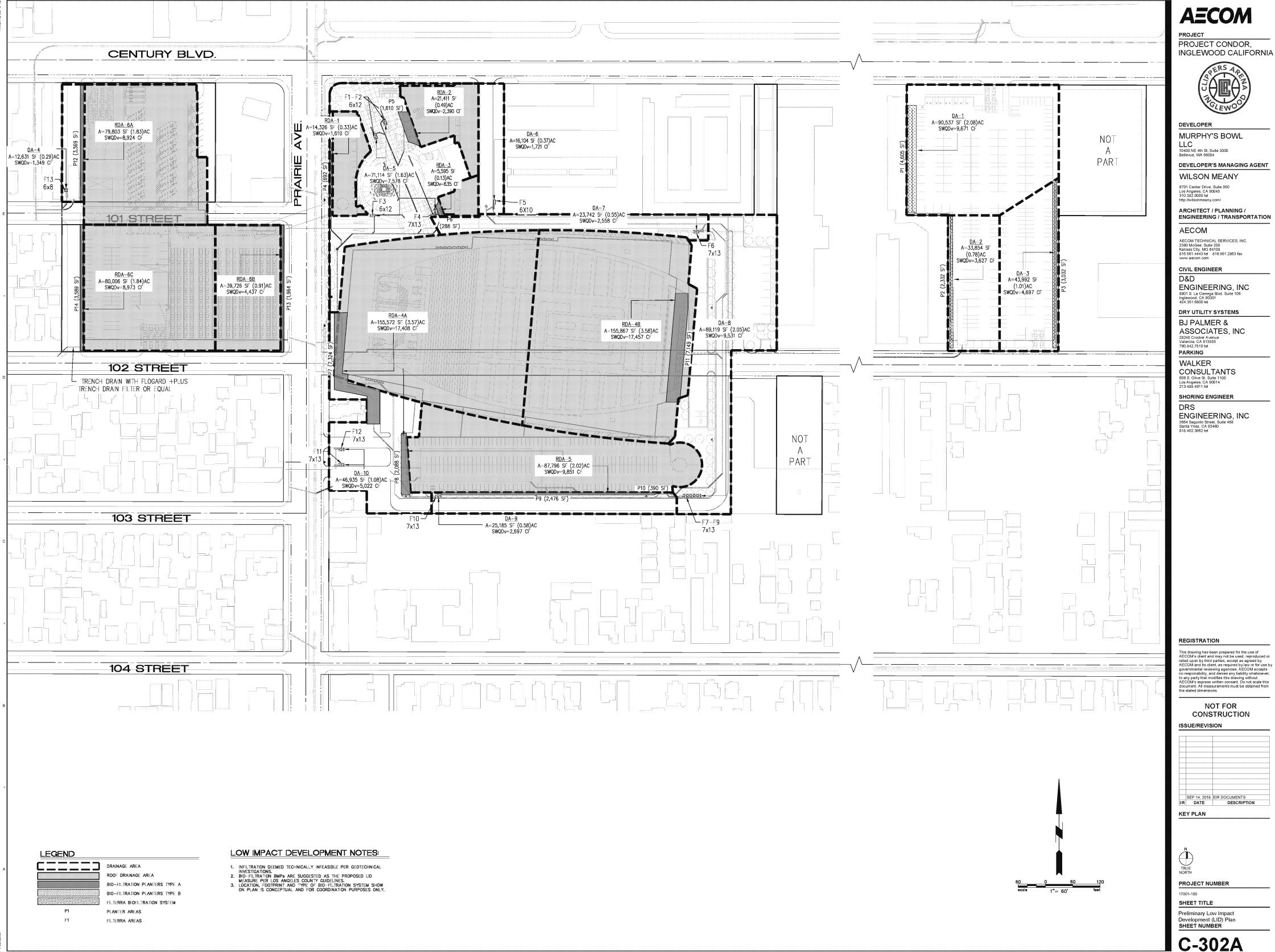
Figure 3 — Site Specific Bio-Filtration Details

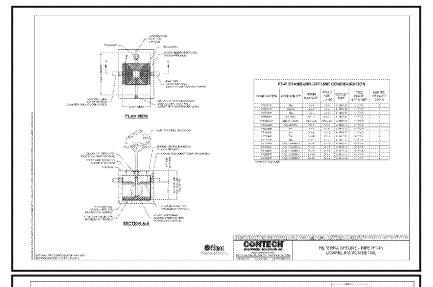


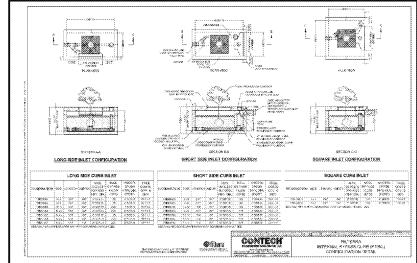
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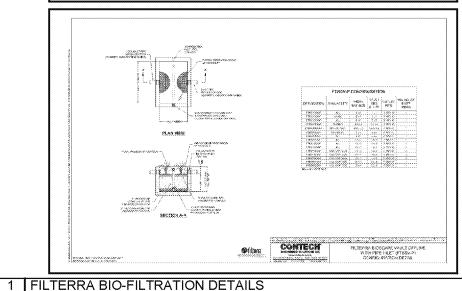
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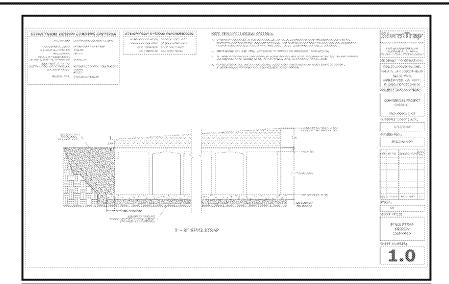
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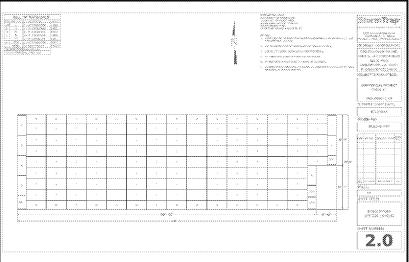


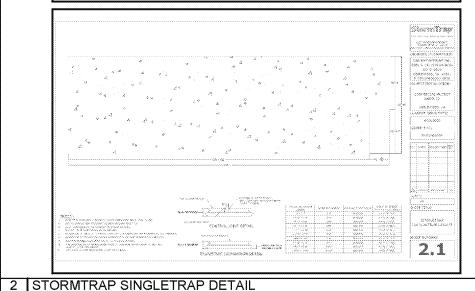


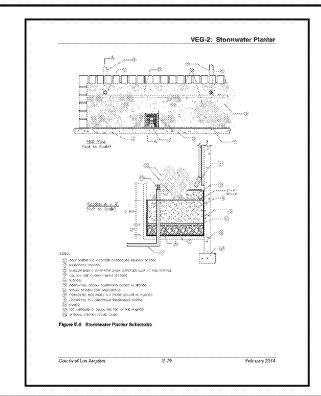




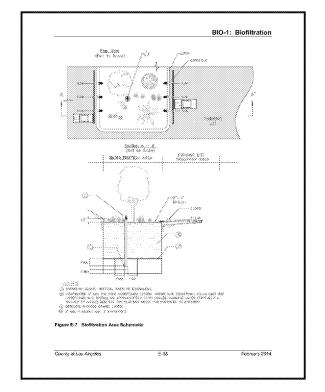








3 BIO-FILTRATION PLANTER - TYPE A



4 BIO-FILTRATION PLANTER - TYPE B

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SITE SPECIFIC BIO-FILTRATION DETAILS FIGURE 3

Filtration Details.dwg

AS SHOWN DATE: 07/31/2018

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Appendix A

Excerpt from Geotechnical Report

PRELIMINARY GEOTECHNICAL INVESTIGATION PROJECT CONDOR SW CORNER OF PRAIRIE AVENUE & W. CENTURY BOULEVARD INGLEWOOD, CALIFORNIA JULY 6, 2018

5.11.1 Flexible Pavement Thicknesses

The following flexible pavement thicknesses for Traffic Index (TI) values of 5, 6 and 7 may be used:

Table 8 - Minimum Flexible (AC) Pavement Thicknesses

Pavement Section (feel)

	(30)		
Traffic Index (TI)	Asphallic Concrete	Aggregate Base	
4 to 5	0.3	0.55	
6 to 7	0.4	0.65	
7 to 8	0.5	0.75	

5.11.2 Concrete Flatwork / Hardscape and Sidewalks

For PCC pavements in pedestrian areas, a pavement section of 4 inches PCC over 6 inches of aggregate base is typical for the kinds of soils to be expected at the site.

It should be noted that the above recommendations apply to parking lot, driveway and street areas only. Loading docks and trash enclosures should be paved with PCC pavement. We recommend that the section consist of a minimum of 6 inches of reinforced Portland cement concrete over 4 inches of Caltrans Class 2 Base with a minimum R-value of 78. The aggregate base should be compacted to at least 95 percent of the maximum dry density per ASTM D-1557 over unyielding subgrade.

5.12 INFILTRATION FEASIBILITY

Preliminary percolation tests were conducted at five (5) selected locations at the site (P-1 through P-5). The results of percolation testing are summarized in Appendix D.

Based on the results, infiltration rates for the soils in the upper 10 feet ranged from 0.32 to 3.52 in/hr. The test results represent a sampling of the upper materials which consist of variable and predominately clayey and silty sands. The upper value may be due to localized presence of more granular soils at the particular test location (P-2).

However, as discussed in this report, the subsurface native soils at the site consist predominately of clayey soils with estimated infiltration rates lower than 0.3 in/hr and with few or no connectivity to permeable soil horizons of adequate thickness. Moreover, the underlying, predominately clayey soils have never experienced saturation and have been found to exhibit more compressibility when inundated; therefore any infiltration of water into the subsurface soils, particularly within the areas to be occupied by permanent structures, is highly discouraged from a foundation performance stand-point. Given these constraints, infiltration practices might not be feasible at the site.



Appendix B

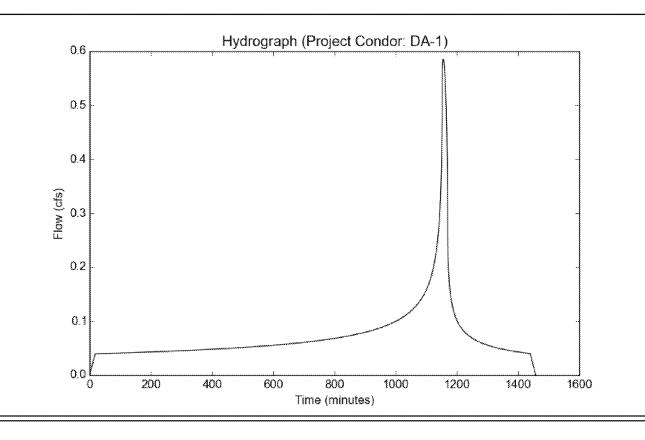
Post-Development Hydrological Conditions

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Input	Para	meters
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Project Name	Project Condor
Subarea ID	DA-1
Area (ac)	2.08
Flow Path Length (ft)	315.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Nooulto		
Modeled (85th percentile storm) Rainfall Dept	h (in) 1.05	
Peak Intensity (in/hr)	0.3431	
Undeveloped Runoff Coefficient (Cu)	0.1	
Developed Runoff Coefficient (Cd)	0.82	
Time of Concentration (min)	18.0	
Clear Peak Flow Rate (cfs)	0.5852	
Burned Peak Flow Rate (cfs)	0.5852	
24-Hr Clear Runoff Volume (ac-ft)	0.148	
24-Hr Clear Runoff Volume (cu-ft)	6447.1944	

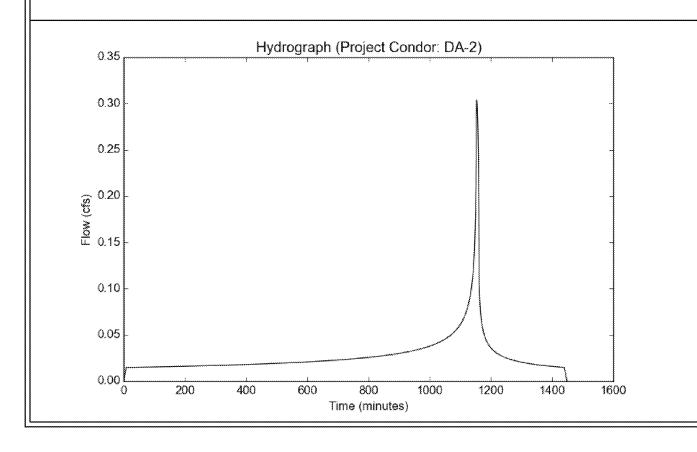


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Input	Parame	ters
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Project Name	Project Condor
Subarea ID	DA-2
Area (ac)	0.78
Flow Path Length (ft)	100.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

output i toodito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.4752
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	9.0
Clear Peak Flow Rate (cfs)	0.304
Burned Peak Flow Rate (cfs)	0.304
24-Hr Clear Runoff Volume (ac-ft)	0.0555
24-Hr Clear Runoff Volume (cu-ft)	2417.6905

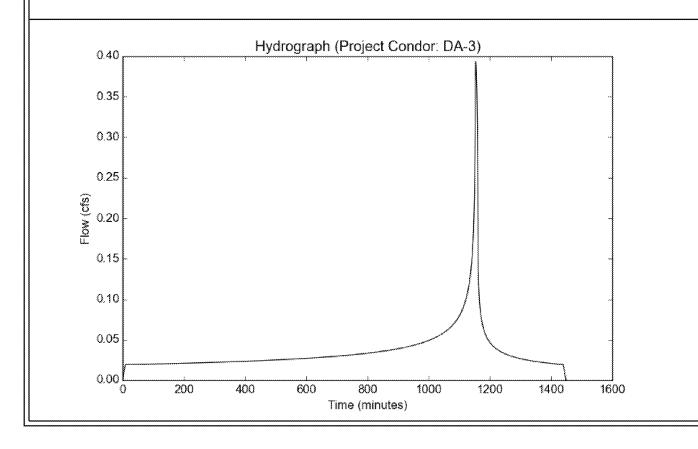


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Input	Param	eters
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Project Name	Project Condor
Subarea ID	DA-3
Area (ac)	1.01
Flow Path Length (ft)	110.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

output i toodito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.4752
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	9.0
Clear Peak Flow Rate (cfs)	0.3936
Burned Peak Flow Rate (cfs)	0.3936
24-Hr Clear Runoff Volume (ac-ft)	0.0719
24-Hr Clear Runoff Volume (cu-ft)	3130.5992

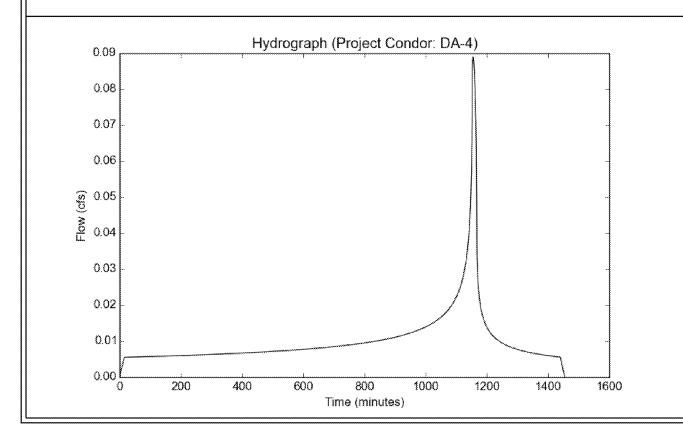


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Input	Parar	neters
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Project Name	Project Condor
Subarea ID	DA-4
Area (ac)	0.29
Flow Path Length (ft)	245.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

output i toodito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.3738
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	15.0
Clear Peak Flow Rate (cfs)	0.0889
Burned Peak Flow Rate (cfs)	0.0889
24-Hr Clear Runoff Volume (ac-ft)	0.0206
24-Hr Clear Runoff Volume (cu-ft)	898.8866

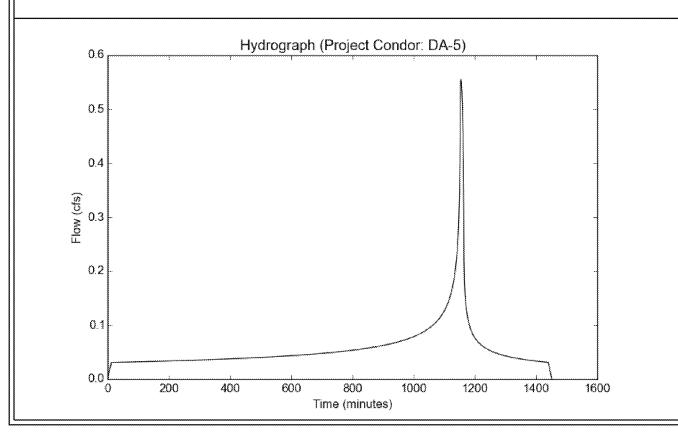


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Input Parameters

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Project Name	Project Condor
Subarea ID	DA-5
Area (ac)	1.63
Flow Path Length (ft)	175.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Modulio	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.4151
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	12.0
Clear Peak Flow Rate (cfs)	0.5549
Burned Peak Flow Rate (cfs)	0.5549
24-Hr Clear Runoff Volume (ac-ft)	0.116
24-Hr Clear Runoff Volume (cu-ft)	5052.3572

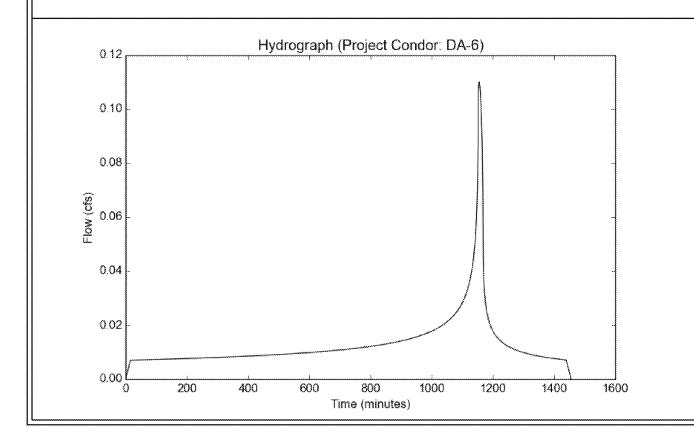


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Input	Para	meters
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Project Name	Project Condor
Subarea ID	DA-6
Area (ac)	0.37
Flow Path Length (ft)	260.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Modulio	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.3626
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	16.0
Clear Peak Flow Rate (cfs)	0.11
Burned Peak Flow Rate (cfs)	0.11
24-Hr Clear Runoff Volume (ac-ft)	0.0263
24-Hr Clear Runoff Volume (cu-ft)	1146.8557

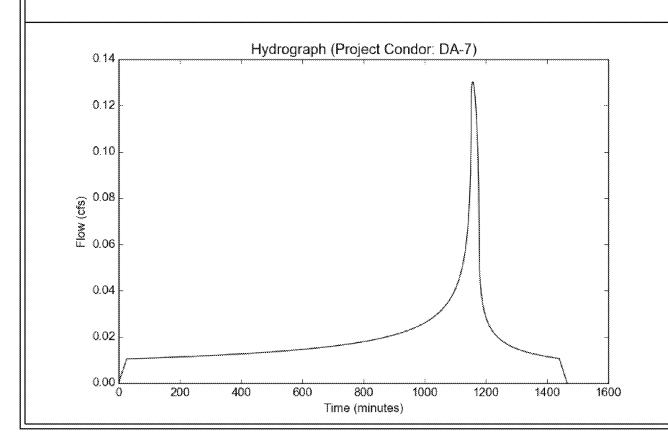


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Input	Para	met	ers
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Project Name	Project Condor
Subarea ID	DA-7
Area (ac)	0.55
Flow Path Length (ft)	575.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Modeled (85th percentile storm) Rainfall Depth (in) 1.05
Peak Intensity (in/hr)	0.2886
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	26.0
Clear Peak Flow Rate (cfs)	0.1302
Burned Peak Flow Rate (cfs)	0.1302
24-Hr Clear Runoff Volume (ac-ft)	0.0391
24-Hr Clear Runoff Volume (cu-ft)	1704.7947

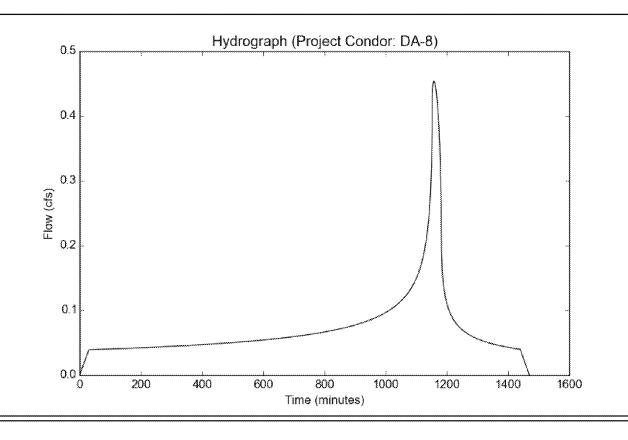


File location: M:/17001/Eng/17001/Hm/LID/Site Plan A/Project Condor Report.pdf Version: HydroCalc 1.0.3

Input	Param	eters
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Project Name	Project Condor
Subarea ID	DA-8
Area (ac)	2.05
Flow Path Length (ft)	700.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Modulio	
Modeled (85th percentile storm) Rainfall Depth	(in) 1.05
Peak Intensity (in/hr)	0.2699
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	30.0
Clear Peak Flow Rate (cfs)	0.4537
Burned Peak Flow Rate (cfs)	0.4537
24-Hr Clear Runoff Volume (ac-ft)	0.1459
24-Hr Clear Runoff Volume (cu-ft)	6354.253

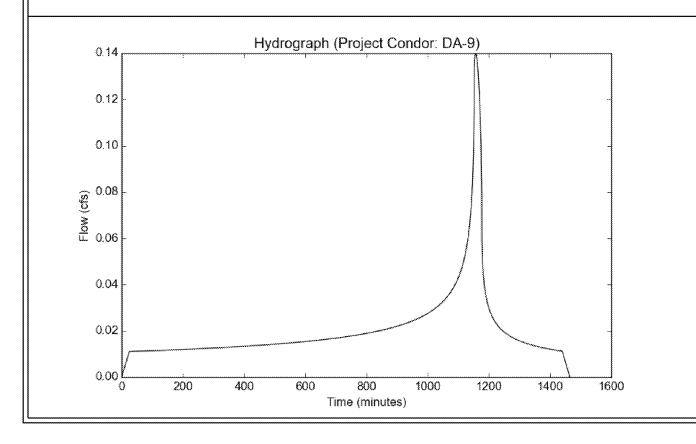


File location: M:/17001/Eng/17001/Hm/LID/Site Plan A/Project Condor Report.pdf Version: HydroCalc 1.0.3

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Project Name	Project Condor
Subarea ID	DA-9
Area (ac)	0.58
Flow Path Length (ft)	530.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Modulio	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.294
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	25.0
Clear Peak Flow Rate (cfs)	0.1398
Burned Peak Flow Rate (cfs)	0.1398
24-Hr Clear Runoff Volume (ac-ft)	0.0413
24-Hr Clear Runoff Volume (cu-ft)	1797.7823

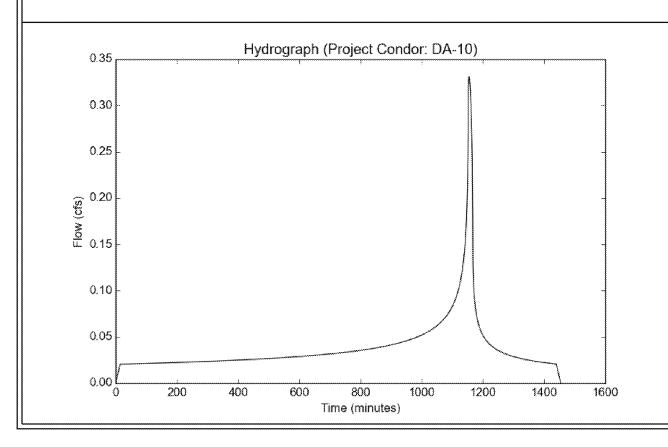


File location: M:/17001/Eng/17001/Hm/LID/Site Plan A/Project Condor Report.pdf Version: HydroCalc 1.0.3

Input	Parar	neters
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Project Name	Project Condor
Subarea ID	DA-10
Area (ac)	1.08
Flow Path Length (ft)	250.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.9
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Modeled (85th percentile storm) Rainfall Depth (i	n) 1.05
Peak Intensity (in/hr)	0.3738
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.82
Time of Concentration (min)	15.0
Clear Peak Flow Rate (cfs)	0.331
Burned Peak Flow Rate (cfs)	0.331
24-Hr Clear Runoff Volume (ac-ft)	0.0768
24-Hr Clear Runoff Volume (cu-ft)	3347.5775

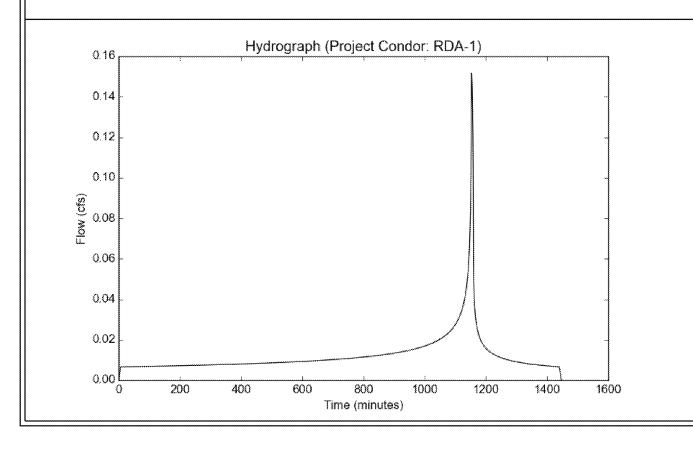


File location: M:/17001/Eng/17001/Hm/LID/Site Plan A/Project Condor Report.pdf Version: HydroCalc 1.0.3

Input	Para	meters
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Project Name	Project Condor
Subarea ID	RDA-1
Area (ac)	0.33
Flow Path Length (ft)	90.0
Flow Path Slope (vft/hft)	0.02
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

output : toouito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.5348
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	7.0
Clear Peak Flow Rate (cfs)	0.1518
Burned Peak Flow Rate (cfs)	0.1518
24-Hr Clear Runoff Volume (ac-ft)	0.0246
24-Hr Clear Runoff Volume (cu-ft)	1072.7647

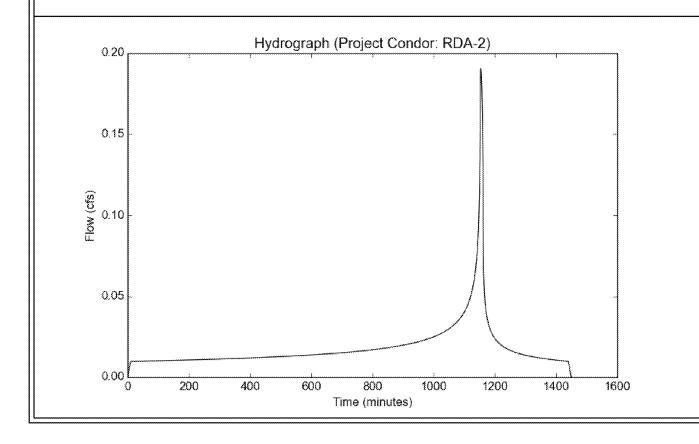


File location: M:/17001/Eng/17001/Hm/LID/Site Plan A/Project Condor Report.pdf Version: HydroCalc 1.0.3

Input Parameters

Project Name	Project Condor
Subarea ID	RDA-2
Area (ac)	0.49
Flow Path Length (ft)	160.0
Flow Path Slope (vft/hft)	0.02
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output 1.00uito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.4523
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	10.0
Clear Peak Flow Rate (cfs)	0.1906
Burned Peak Flow Rate (cfs)	0.1906
24-Hr Clear Runoff Volume (ac-ft)	0.0366
24-Hr Clear Runoff Volume (cu-ft)	1592.894

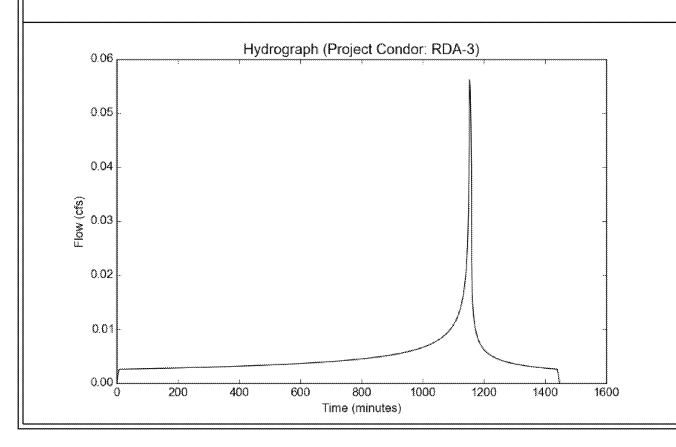


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Input	Parar	neters
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Project Name	Project Condor
Subarea ID	RDA-3
Area (ac)	0.13
Flow Path Length (ft)	110.0
Flow Path Slope (vft/hft)	0.02
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Modulio	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.5023
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	8.0
Clear Peak Flow Rate (cfs)	0.0562
Burned Peak Flow Rate (cfs)	0.0562
24-Hr Clear Runoff Volume (ac-ft)	0.0097
24-Hr Clear Runoff Volume (cu-ft)	422.6043

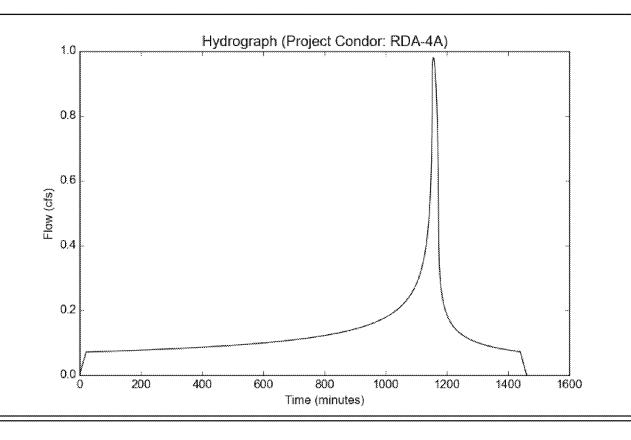


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Input	Para	meters
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Project Name	Project Condor
Subarea ID	RDA-4A
Area (ac)	3.57
Flow Path Length (ft)	510.0
Flow Path Slope (vft/hft)	0.02
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

output i toodito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.3191
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	21.0
Clear Peak Flow Rate (cfs)	0.9798
Burned Peak Flow Rate (cfs)	0.9798
24-Hr Clear Runoff Volume (ac-ft)	0.2664
24-Hr Clear Runoff Volume (cu-ft)	11605.4209

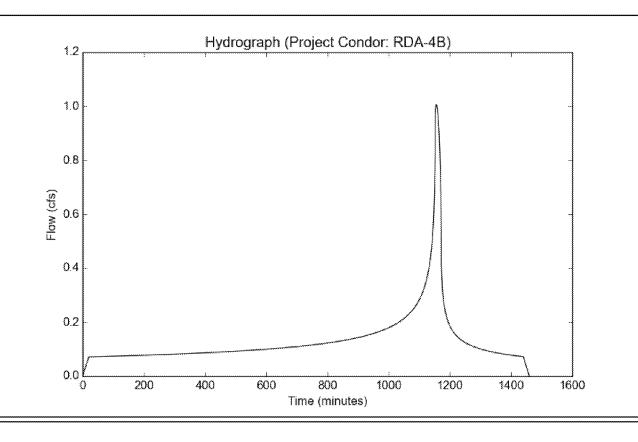


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Input	Para	meters
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Project Name	Project Condor
Subarea ID	RDA-4B
Area (ac)	3.58
Flow Path Length (ft)	470.0
Flow Path Slope (vft/hft)	0.02
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output : (Oodito	
Modeled (85th percentile storm) Rainfall Depth (in) 1.05
Peak Intensity (in/hr)	0.3265
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	20.0
Clear Peak Flow Rate (cfs)	1.0053
Burned Peak Flow Rate (cfs)	1.0053
24-Hr Clear Runoff Volume (ac-ft)	0.2672
24-Hr Clear Runoff Volume (cu-ft)	11637.923

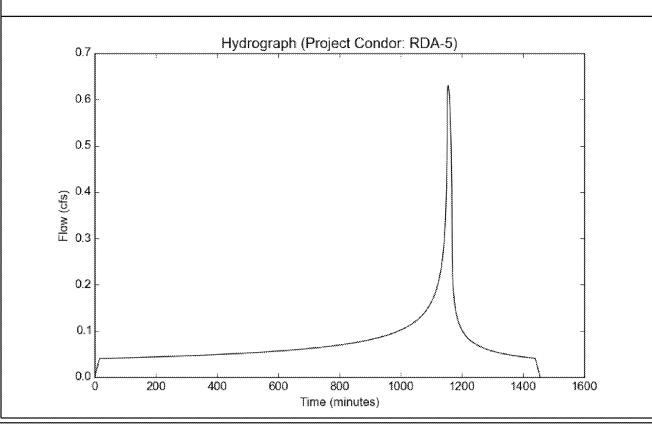


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Input Parameters

mpat i arametero	
Project Name	Project Condor
Subarea ID	RDA-5
Area (ac)	2.02
Flow Path Length (ft)	340.0
Flow Path Slope (vft/hft)	0.02
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

- apart i courte	
Modeled (85th percentile storm) Rainfall Dept	h (in) 1.05
Peak Intensity (in/hr)	0.3626
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	16.0
Clear Peak Flow Rate (cfs)	0.63
Burned Peak Flow Rate (cfs)	0.63
24-Hr Clear Runoff Volume (ac-ft)	0.1507
24-Hr Clear Runoff Volume (cu-ft)	6566.6372

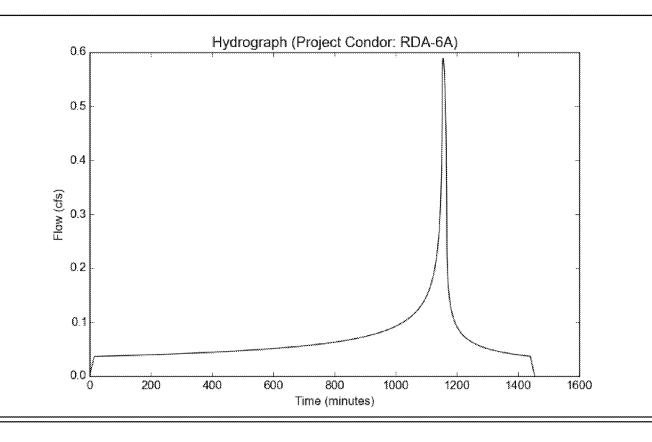


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Input	Param	eters
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Project Name	Project Condor	
Subarea ID	RDA-6A	
Area (ac)	1.83	
Flow Path Length (ft)	310.0	
Flow Path Slope (vft/hft)	0.02	
85th Percentile Rainfall Depth (in)	1.05	
Percent Impervious	0.95	
Soil Type	13	
Design Storm Frequency	85th percentile storm	
Fire Factor	0	
LID	True	

Output Hoodito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.3738
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	15.0
Clear Peak Flow Rate (cfs)	0.5883
Burned Peak Flow Rate (cfs)	0.5883
24-Hr Clear Runoff Volume (ac-ft)	0.1366
24-Hr Clear Runoff Volume (cu-ft)	5948.9809

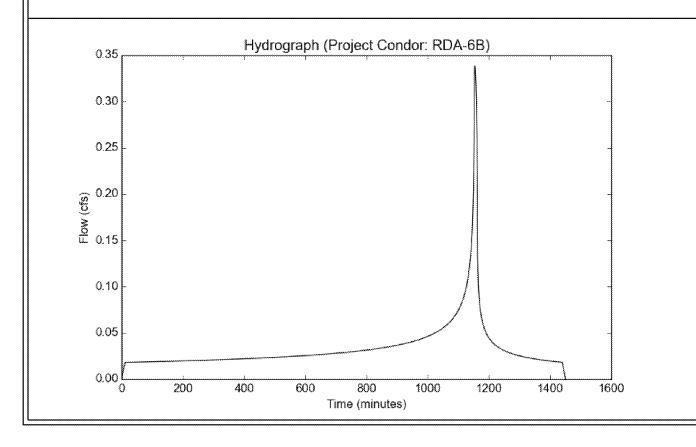


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Input	Param	eters
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Project Name	Project Condor
Subarea ID	RDA-6B
Area (ac)	0.91
Flow Path Length (ft)	190.0
Flow Path Slope (vft/hft)	0.02
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Value 1/05/2 CT / ND 1/1/10 CT	(; \
Modeled (85th percentile storm) Rainfall Depth	
Peak Intensity (in/hr)	0.4325
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	11.0
Clear Peak Flow Rate (cfs)	0.3384
Burned Peak Flow Rate (cfs)	0.3384
24-Hr Clear Runoff Volume (ac-ft)	0.0679
24-Hr Clear Runoff Volume (cu-ft)	2958.2325

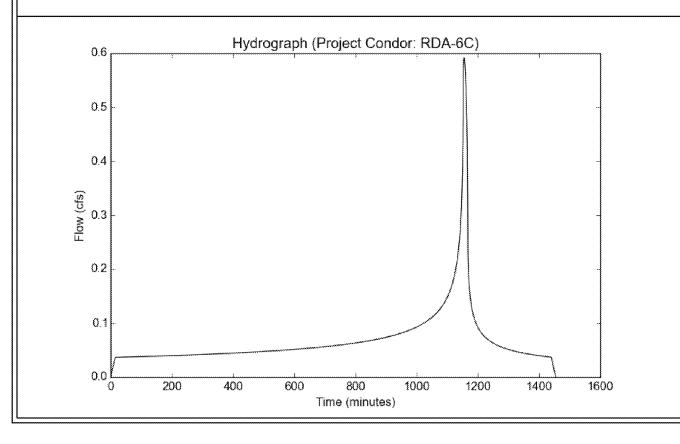


File location: M:/17001/Eng/17001/Hm/LID/Site Plan A/Project Condor Report.pdf Version: HydroCalc 1.0.3

Input Parameters

Project Name	Project Condor	
Subarea ID	RDA-6C	
Area (ac)	1.84	
Flow Path Length (ft)	320.0	
Flow Path Slope (vft/hft)	0.02	
85th Percentile Rainfall Depth (in)	1.05	
Percent Impervious	0.95	
Soil Type	13	
Design Storm Frequency	85th percentile storm	
Fire Factor	0	
LID	True	

output i toodito	
Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.3738
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	15.0
Clear Peak Flow Rate (cfs)	0.5915
Burned Peak Flow Rate (cfs)	0.5915
24-Hr Clear Runoff Volume (ac-ft)	0.1373
24-Hr Clear Runoff Volume (cu-ft)	5981.489





Appendix C

Bio-Filtration Sizing Calculations

LID SUMMARY TABLE

AREA

SUBAREA	SF	ACRE	Vm	Vdesign	Qpm	Amin	BMP Provided
DA-1	90,537	2.08	6447	9671	0.5852	3,868	PLANTER B
DA-2	33,854	0.78	2418	3627	0.3040	1,451	PLANTER B
DA-3	43,992	1.01	3131	4697	0.3936	1,879	PLANTER B
DA-4	12,631	0.29	899	1349	0.0889	43	FILTERRA
DA-5	71,114	1.63	5052	7578	0.5549	256	FILTERRA
DA-6	16,104	0.37	1147	1721	0.1100	55	FILTERRA
DA-7	23,742	0.55	1705	2558	0.1302	73	FILTERRA
DA-8	89,119	2.05	6354	9531	0.4537	264	FILTERRA
DA-9	25,185	0.58	1798	2697	0.1398	78	FILTERRA
DA-10	46,835	1.08	3348	5022	0.3310	160	FILTERRA
RDA-1	14,326	0.33	1073	1610	0.1518	644	PLANTER A
RDA-2	21,411	0.49	1593	2390	0.1906	956	PLANTER A
RDA-3	5,595	0.13	423	635	0.0562	254	PLANTER A
RDA-4A	155,572	3.57	11605	17408	0.9798	6,963	PLANTER A
RDA-4B	155,867	3.58	11638	17457	1.0053	6,983	PLANTER A
RDA-5	87,796	2.02	6567	9851	0.6300	3,940	PLANTER A
RDA-6A	79,803	1.83	5949	8924	0.5883	3,569	PLANTER A
RDA-6B	39,726	0.91	2958	4437	0.3384	1,775	PLANTER A
RDA-6C	80,006	1.84	5981	8972	0.5915	3,589	PLANTER A

PROJECT CONDOR

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

DA-1

Ρ1

Site area:	90,537	sf
Impervious	0.90	%
85th Percentile:	1.05	in
Volume (V _m):	6447	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	9671	cf

Note: For Flow Through Planters

$V_{design} = 1.5*Vm$

Sizing	Units	
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/FS)$	6	in/hour
Т	3	hrs
$H_{planter}$	51	in
d _p	12	in
A _{min} =	3,868	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} +} d_p$$
12

A_{min} = Minimum Area Required

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DRAINAGE AREA

<u>PLANTER</u>

DA-2

P2

Site area:	33,854	sf
Impervious	0.90	%
85th Percentile:	1.05	in
Volume (V _m):	2418	cf
$V_{\rm design} = V_{\rm m} * 1.5$	3627	cf

Note: For Flow Through Planters

$V_{design} = 1.5*Vm$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Т	3	hrs
$H_{planter}$	51	in
d _p	12	in
A _{min} =	1,450.8	sf

$$\label{eq:Amin} Amin = \frac{V_{design}}{T*K_{sat,des}+} \frac{12}{d_p}$$

$$T= \qquad \qquad Drawdown\ Time$$

$$H_{planter} = \qquad Planter\ Height$$

$$d_p = \qquad Ponding\ Depth$$

Minimum Area Required

 $A_{min} =$

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DRAINAGE AREA

<u>PLANTER</u>

DA-3

Р3

Site area:	43,992	sf
Impervious	0.90	%
85th Percentile:	1.05	in
Volume (V _m):	3131	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	4697	cf

Note: For Flow Through Planters

$V_{design} = 1.5*Vm$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/FS)$	6	in/hour
Т	3	hrs
H _{planter}	57	in
d _p	12	in
A _{min} =	1,878.6	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} + d_p}$$

$$\frac{12}{}$$

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DRAINAGE AREA

<u>PLANTER</u>

RDA-1

Ρ4

Site area:	14,326	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	1073	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	1610	cf

Note: For Flow Through Planters

$V_{design} = 1.5*Vm$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Τ	3	hrs
$H_{planter}$	51	in
d _p	12	in
A _{min} =	643.8	sf

Amin =
$$V_{design}$$

$$\frac{T * K_{sat,des} +}{12} d_p$$

T = Drawdown Time $H_{planter} = Planter Height$ $d_p = Ponding Depth$

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-2

P5

Site area:	21,411	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	1593	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	2390	cf

Note: For Flow Through Planters

$V_{design} = 1.5*Vm$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/FS)$	6	in/hour
Т	3	hrs
$H_{planter}$	57	in
d _p	12	in
A _{min} =	955.8	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} + d_p}$$
12

Drawdown Time

 $T= \qquad \qquad \text{Drawdown Time} \\ H_{planter} = \qquad \qquad \text{Planter Height} \\ d_p = \qquad \qquad \text{Ponding Depth} \\$

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-3

Р6

Site area:	5,595	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	423	cf
$V_{design} = V_m * 1.5$	635	cf

Note: For Flow Through Planters

$V_{design} = 1.5*Vm$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/FS)$	6	in/hour
Т	3	hrs
H _{planter}	57	in
d _p	12	in
A _{min} =	253.8	sf

Minimum Area Required

T=

 $d_p =$

 $A_{min} =$

 $H_{planter} =$

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-4A

P7, P8

Site area:	155,572	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	11605	cf
$V_{design} = V_m * 1.5$	17408	cf

Note: For Flow Through Planters

$V_{design} = 1.5*Vm$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Т	3	hrs
$H_{planter}$	51	in
d _p	12	in
A _{min} =	6,963.0	sf

Amin =
$$V_{design}$$

$$T * K_{sat,des} + d_p$$

$$12$$

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-4B

P11

Site area:	155,867	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	11638	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	17457	cf

Note: For Flow Through Planters

$$V_{design} = 1.5*Vm$$

Sizing	Units	
K _{sat} 12		in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Т	3	hrs
H _{planter}	51	in
d _p	12	in
A _{min} =	6,982.8	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} + d_p}$$

$$12$$

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-5

P9, 10

Site area:	87,796	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	6567	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	9851	cf

Note: For Flow Through Planters

$$V_{design} = 1.5*Vm$$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Т	3	hrs
$H_{planter}$	51	in
d _p	12	in
A _{min} =	3,940.2	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} + d_p}$$
12

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-6A

P12

Site area:	79,803	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	5949	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	8924	cf

Note: For Flow Through Planters

$$V_{design} = 1.5*Vm$$

Sizing	Units	
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Т	3	hrs
$H_{planter}$	51	in
d _p	12	in
A _{min} =	3,569.4	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} + d_p}$$

$$12$$

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-6B

P13

Site area:	39,726	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	2958	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	4437	cf

Note: For Flow Through Planters

$$V_{design} = 1.5*Vm$$

Sizing		Units
K _{sat}	12	in/hour
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Т	3	hrs
$H_{planter}$	51	in
d _p	12	in
A _{min} =	1,774.8	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} + d_p}$$
12

INGLEWOOD, CA

DRAINAGE AREA

<u>PLANTER</u>

RDA-6C

P14

Site area:	80,006	sf
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V _m):	5981	cf
$V_{\text{design}} = V_{\text{m}} * 1.5$	8972	cf

Note: For Flow Through Planters

$$V_{design} = 1.5*Vm$$

Sizing	Units	
K _{sat}	K _{sat} 12	
FS	2	-
$K_{\text{sat,des}} = (K_{\text{sat}}/\text{FS})$	6	in/hour
Т	3	hrs
H _{planter}	51	in
d _p	12	in
A _{min} =	3,588.6	sf

Amin =
$$\frac{V_{design}}{T * K_{sat,des} + d_p}$$

$$12$$





Applicable in the Area Goverened by the Los Angeles County MS4 Permit (NPDES PERMIT NO. CASO04001; ORDER NO. R4-2012-0175)

For final design please contact:

Alexandra Dubrock - Stormwater Consultant

adubrock@conteches.com

Phone: 949-217-4663

Contact Information		Project Information	
Engineer of Record Name	Robert Dizon	Project Name	Condor
Engineer of Record Company Name	D&D Engineering, Inc.	Project Location	Inglewood, CA
Engineer of Record Office Zip Code	90301	Catchment Name	DA-4
Drainage Area Inputs			
Drainage Area		12631	ft ⁻
Runoff coefficient		0.9	-
Time of concentration		15	min
Long term reliable infiltration rate		0.09	in/hr
85th percentile, 24-hour depth (see hype	rlink below)	1.05	in
LA County Rainfall Depth Analysis			
Filterra Configuration (Select from Dr	op-Down)	Internal Bypass Curb	
Refer to "Filterra Configurations" tab for o	descriptions and standard detai	ls for download.	
Constants			
LAX Airport 85th Percentile, 24-hour dept	:h (for reference only)	1.02	in
Filterra hydraulic loading capacity		1.45	gpm/ft²
<u>Outputs</u>			
Stormwater Quality Design Volume		995	ft ³
Design Rainfall Intensity for Equivalent Lo	ng Term Capture	0.359	in/hr
Site Scaling Factor		1.03	-
Stormwater Quality Design Flow Rate		0.10	cfs
Design Alternatives Available		Stand Alone Filterra Permitted	
Design Recommendations			
Primary Recommendation - Stand Alor	<u>ne Filterra</u>		
Adjusted Filterra Design Intensity		0.514	in/hr
Stormwater Quality Design Flow Rate		0.14	cfs
Required Filterra Area		43	ft ²
Filterra Model ID		FTIBC 6x8 / 8x6	
Alternative Recommendation - Filterra	ı + Infiltration Storage		. 7
Required Filterra Area		31	ft ²
Filterra Model ID		FTIBC 4x8 / 8x4	. 3
ChamberMaxx volume		133	ft ³
ChamberMaxx count		2	chambers

^{1.} Filterra systems must be designed and sized following the methodology in Section 4 of the August 2015 report prepared by Geosyntec Consultants, entitled "Filterra Equivalency Analysis and Design Criteria" which is the basis for this design tool.

^{2.} Filterra systems use an engineered biofiltration media. Filterra systems, including the engineered biofiltration media, must be provided by the manufacturer. No substitution of materials/media is allowed.

^{3.} Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv onsite.

^{4.} Hydromodification requirements of Section VI.D.7.c.iv of the Los Angeles County MS4 Permit must be considered separately regardless of what type of biofiltration is used.

^{5.} Operation and maintenance of Filterra systems must be conducted consistent with the recommendations in the Filterra maintenance manual provided by Contech Engineered Solutions.

^{6.} In the area governed by the Los Angeles Region Phase I stormwater permit, conventional biofilters must be sized to treat 1.5X the SWQDV. This results in an average annual capture rate of 93%. Filterra systems sized using this tool will also treat at least 93% of the average annual runoff volume.





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Phone: 949-217-4663

Contact Information		Project Information	
Engineer of Record Name	Robert Dizon	Project Name	Condor
Engineer of Record Company Name	D&D Engineering, Inc.	Project Location	Inglewood, CA
Engineer of Record Office Zip Code	90301	Catchment Name	DA-5
Drainage Area Inputs			
Drainage Area		71114	ft ⁻
Runoff coefficient		0.9	-
Time of concentration		12	min
Long term reliable infiltration rate		0.09	in/hr
85th percentile, 24-hour depth (see hype	rlink below)	1.05	in
LA County Rainfall Depth Analysis			
Filterra Configuration (Select from D	rop-Down)	Peak Diversion	
Refer to "Filterra Configurations" tab for	descriptions and standard detai	ls for download.	
Constants			
LAX Airport 85th Percentile, 24-hour dep	th (for reference only)	1.02	in
Filterra hydraulic loading capacity		1.45	gpm/ft ²
<u>Outputs</u>			<u>-</u>
Stormwater Quality Design Volume		5,600	ft ³
Design Rainfall Intensity for Equivalent Lo	ong Term Capture	0.372	in/hr
Site Scaling Factor	,	1.03	- -
Stormwater Quality Design Flow Rate		0.57	cfs
Design Alternatives Available		Stand Alone Filterra Permitted	
Design Recommendations			
Primary Recommendation - Stand Alo	ne Filterra		
Adjusted Filterra Design Intensity		0.542	in/hr
Stormwater Quality Design Flow Rate		0.83	cfs
Required Filterra Area		256	ft ²
Filterra Model ID		See Note	
l	system. Consider a different Filterra co	nfiguration, utilizing multiple structures, or utilizing	ng Filterra Bioscape. Contact Contech
Alternative Recommendation - Filtern	a + Infiltration Storage		
Required Filterra Area		176	ft ²
Filterra Model ID		See Note	
ChamberMaxx volume		750	ft ³
ChamberMaxx count		10	chambers
	system. Consider a different Filterra co	nfiguration, utilizing multiple structures, or utilizing	ng Filterra Bioscape. Contact Contech
for more info.			

- 1. Filterra use is Subject to the following conditions:

 1. Filterra systems must be designed and sized following the methodology in Section 4 of the August 2015 report prepared by Geosyntec Consultants, entitled "Filterra Equivalency Analysis and Design
- Criteria" which is the basis for this design tool.
 2. Filterra systems use an engineered biofiltration media. Filterra systems, including the engineered biofiltration media, must be provided by the manufacturer. No substitution of materials/media is
- allowed.

 3. Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv on-
- 3. Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv or site.
- 4. Hydromodification requirements of Section VI.D.7.c.iv of the Los Angeles County MS4 Permit must be considered separately regardless of what type of biofiltration is used.
- 5. Operation and maintenance of Filterra systems must be conducted consistent with the recommendations in the Filterra maintenance manual provided by Contech Engineered Solutions.
- 6. In the area governed by the Los Angeles Region Phase I stormwater permit, conventional biofilters must be sized to treat 1.5X the SWQDV. This results in an average annual capture rate of 93%. Filterra systems sized using this tool will also treat at least 93% of the average annual runoff volume.





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For final design please contact:

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Phone: 949-217-4663

Contact Information		Project Information	
Engineer of Record Name	Robert Dizon	Project Name	Condor
Engineer of Record Company Name	D&D Engineering, Inc.	Project Location	Inglewood, CA
Engineer of Record Office Zip Code	90301	Catchment Name	DA-6
Drainage Area Inputs			
Drainage Area		16104	ft ⁻
Runoff coefficient		0.9	-
Time of concentration		16	min
Long term reliable infiltration rate		0.09	in/hr
85th percentile, 24-hour depth (see hyper	link below)	1.05	in
LA County Rainfall Depth Analysis			
Filterra Configuration (Select from Dr	op-Down)	Internal Bypass Curb	
Refer to "Filterra Configurations" tab for o	lescriptions and standard detai	ls for download.	00000000000000000000000000000000000000
<u>Constants</u>			
LAX Airport 85th Percentile, 24-hour dept	h (for reference only)	1.02	in
Filterra hydraulic loading capacity		1.45	gpm/ft ²
<u>Outputs</u>			
Stormwater Quality Design Volume		1,268	ft ³
Design Rainfall Intensity for Equivalent Long Term Capture		0.355	in/hr
Site Scaling Factor		1.03	=
Stormwater Quality Design Flow Rate		0.12	cfs
Design Alternatives Available		Stand Alone Filterra Permitted	
Design Recommendations			
Primary Recommendation - Stand Alor	ne Filterra		
Adjusted Filterra Design Intensity		0.508	in/hr
Stormwater Quality Design Flow Rate		0.18	cfs
Required Filterra Area		54	ft ²
Filterra Model ID		FTIBC 6x10 / 10x6	
Alternative Recommendation - Filterra	+ Infiltration Storage	,	. 7
Required Filterra Area		38	ft ²
Filterra Model ID		FTIBC 6x8 / 8x6	. 3
ChamberMaxx volume		170	ft ³
ChamberMaxx count		3	chambers

^{1.} Filterra systems must be designed and sized following the methodology in Section 4 of the August 2015 report prepared by Geosyntec Consultants, entitled "Filterra Equivalency Analysis and Design Criteria" which is the basis for this design tool.

^{2.} Filterra systems use an engineered biofiltration media. Filterra systems, including the engineered biofiltration media, must be provided by the manufacturer. No substitution of materials/media is allowed.

^{3.} Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv onsite.

^{4.} Hydromodification requirements of Section VI.D.7.c.iv of the Los Angeles County MS4 Permit must be considered separately regardless of what type of biofiltration is used.

^{5.} Operation and maintenance of Filterra systems must be conducted consistent with the recommendations in the Filterra maintenance manual provided by Contech Engineered Solutions.

^{6.} In the area governed by the Los Angeles Region Phase I stormwater permit, conventional biofilters must be sized to treat 1.5X the SWQDV. This results in an average annual capture rate of 93%. Filterra systems sized using this tool will also treat at least 93% of the average annual runoff volume.





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For final design please contact:

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adubrock@conteches.com

Phone: 949-217-4663

Contact Information		Project Information	
Engineer of Record Name	Robert Dizon	Project Name	Condor
Engineer of Record Company Name	D&D Engineering, Inc.	Project Location	Inglewood, CA
Engineer of Record Office Zip Code	90301	Catchment Name	DA-7
Drainage Area Inputs			
Drainage Area		23742	ft ⁴
Runoff coefficient		0.9	-
Time of concentration		26	min
Long term reliable infiltration rate		0.09	in/hr
85th percentile, 24-hour depth (see hyper	rlink below)	1.05	in
LA County Rainfall Depth Analysis			
Filterra Configuration (Select from Dr	op-Down)	Internal Bypass Curb	
Refer to "Filterra Configurations" tab for o	descriptions and standard detai	ls for download.	00000000000000000000000000000000000000
<u>Constants</u>			
LAX Airport 85th Percentile, 24-hour dept	h (for reference only)	1.02	in
Filterra hydraulic loading capacity		1.45	gpm/ft ²
<u>Outputs</u>			
Stormwater Quality Design Volume		1,870	ft ³
Design Rainfall Intensity for Equivalent Long Term Capture		0.326	in/hr
Site Scaling Factor		1.03	=
Stormwater Quality Design Flow Rate		0.17	cfs
Design Alternatives Available		Stand Alone Filterra Permitted	
Design Recommendations			
Primary Recommendation - Stand Alor	ne Filterra		
Adjusted Filterra Design Intensity		0.462	in/hr
Stormwater Quality Design Flow Rate		0.24	cfs
Required Filterra Area		73	ft ²
Filterra Model ID		FTIBC 6x12 / 12x6	
Alternative Recommendation - Filterra	+ Infiltration Storage		
Required Filterra Area		52	ft ²
Filterra Model ID		FTIBC 6x10 / 10x6	
ChamberMaxx volume		251	ft ³
Chamber Maxx count		4	chambers

^{1.} Filterra systems must be designed and sized following the methodology in Section 4 of the August 2015 report prepared by Geosyntec Consultants, entitled "Filterra Equivalency Analysis and Design Criteria" which is the basis for this design tool.

^{2.} Filterra systems use an engineered biofiltration media. Filterra systems, including the engineered biofiltration media, must be provided by the manufacturer. No substitution of materials/media is allowed.

^{3.} Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv on-site.

^{4.} Hydromodification requirements of Section VI.D.7.c.iv of the Los Angeles County MS4 Permit must be considered separately regardless of what type of biofiltration is used.

^{5.} Operation and maintenance of Filterra systems must be conducted consistent with the recommendations in the Filterra maintenance manual provided by Contech Engineered Solutions.

^{6.} In the area governed by the Los Angeles Region Phase I stormwater permit, conventional biofilters must be sized to treat 1.5X the SWQDV. This results in an average annual capture rate of 93%. Filterra systems sized using this tool will also treat at least 93% of the average annual runoff volume.





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Phone: 949-217-4663

Contact Information		Project Information	
Engineer of Record Name	Robert Dizon	Project Name	Condor
Engineer of Record Company Name	D&D Engineering, Inc.	Project Location	Inglewood, CA
Engineer of Record Office Zip Code	90301	Catchment Name	DA-8
Drainage Area Inputs			
Drainage Area		89119	ft ⁻
Runoff coefficient		0.9	-
Time of concentration		30	min
Long term reliable infiltration rate		0.09	in/hr
85th percentile, 24-hour depth (see hyper	link below)	1.05	in
LA County Rainfall Depth Analysis		6	
Filterra Configuration (Select from Dro	Filterra Configuration (Select from Drop-Down)		
Refer to "Filterra Configurations" tab for d	lescriptions and standard detai	ls for download.	
Constants			oconnection
LAX Airport 85th Percentile, 24-hour deptl	h (for reference only)	1.02	in
Filterra hydraulic loading capacity		1.45	gpm/ft ²
Outputs			
Stormwater Quality Design Volume		7,018	ft ³
Design Rainfall Intensity for Equivalent Lor	ng Term Capture	0.320	in/hr
Site Scaling Factor		1.03	- -
Stormwater Quality Design Flow Rate		0.61	cfs
Design Alternatives Available		Stand Alone Filterra Permitted	
Design Recommendations			
Primary Recommendation - Stand Alon	e Filterra		
Adjusted Filterra Design Intensity		0.446	in/hr
Stormwater Quality Design Flow Rate		0.85	cfs
Required Filterra Area		264	ft ²
Filterra Model ID		See Note	
Note: Drainage area is too large for single Filterra s	ystem. Consider a different Filterra co	nfiguration, utilizing multiple structures, or utilizing	Filterra Bioscape, Contact Contech
for more info.			
Alternative Recommendation - Filterra	+ Infiltration Storage		
Required Filterra Area		190	ft ²
Filterra Model ID		See Note	
ChamberMaxx volume		940	ft ³
ChamberMaxx count		13	chambers
1	ystem. Consider a different Filterra co	nfiguration, utilizing multiple structures, or utilizing	Filterra Bioscape. Contact Contech
for more info.			

- 1. Filterra systems must be designed and sized following the methodology in Section 4 of the August 2015 report prepared by Geosyntec Consultants, entitled "Filterra Equivalency Analysis and Design Criteria" which is the basis for this design tool.
- 2. Filterra systems use an engineered biofiltration media. Filterra systems, including the engineered biofiltration media, must be provided by the manufacturer. No substitution of materials/media is allowed.
- 3. Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv onsite.
- 4. Hydromodification requirements of Section VI.D.7.c.iv of the Los Angeles County MS4 Permit must be considered separately regardless of what type of biofiltration is used.
- 5. Operation and maintenance of Filterra systems must be conducted consistent with the recommendations in the Filterra maintenance manual provided by Contech Engineered Solutions.
- 6. In the area governed by the Los Angeles Region Phase I stormwater permit, conventional biofilters must be sized to treat 1.5X the SWQDV. This results in an average annual capture rate of 93%. Filterra systems sized using this tool will also treat at least 93% of the average annual runoff volume.





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Phone: 949-217-4663

Contact Information		Project Information	
Engineer of Record Name	Robert Dizon	Project Name	Condor
Engineer of Record Company Name	D&D Engineering, Inc.	Project Location	Inglewood, CA
Engineer of Record Office Zip Code	90301	Catchment Name	DA-9
Drainage Area Inputs			
Drainage Area		25185	ft⁴
Runoff coefficient		0.9	-
Time of concentration		25	min
Long term reliable infiltration rate		0.09	in/hr
85th percentile, 24-hour depth (see hype	rlink below)	1.05	in
LA County Rainfall Depth Analysis			
Filterra Configuration (Select from D	Filterra Configuration (Select from Drop-Down)		
Refer to "Filterra Configurations" tab for	descriptions and standard detai	is for download.	
<u>Constants</u>			
LAX Airport 85th Percentile, 24-hour dep	th (for reference only)	1.02	in
Filterra hydraulic loading capacity		1.45	gpm/ft²
<u>Outputs</u>			
Stormwater Quality Design Volume		1,983	ft ³
Design Rainfall Intensity for Equivalent Lo	ong Term Capture	0.328	in/hr
Site Scaling Factor		1.03	-
Stormwater Quality Design Flow Rate		0.18	cfs
Design Alternatives Available		Stand Alone Filterra Permitted	
Design Recommendations			
Primary Recommendation - Stand Alo	ne Filterra		
Adjusted Filterra Design Intensity		0.466	in/hr
Stormwater Quality Design Flow Rate		0.25	cfs
Required Filterra Area		78	ft ²
Filterra Model ID		FTIBC 7x13 / 13x7	
Alternative Recommendation - Filterr	a + Infiltration Storage		
Required Filterra Area		55	ft ²
Filterra Model ID		FTIBC 6x10 / 10x6	_
ChamberMaxx volume		266	ft ³
ChamberMaxx count		4	chambers

^{1.} Filterra systems must be designed and sized following the methodology in Section 4 of the August 2015 report prepared by Geosyntec Consultants, entitled "Filterra Equivalency Analysis and Design Criteria" which is the basis for this design tool.

^{2.} Filterra systems use an engineered biofiltration media. Filterra systems, including the engineered biofiltration media, must be provided by the manufacturer. No substitution of materials/media is allowed.

^{3.} Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv on-site.

^{4.} Hydromodification requirements of Section VI.D.7.c.iv of the Los Angeles County MS4 Permit must be considered separately regardless of what type of biofiltration is used.

^{5.} Operation and maintenance of Filterra systems must be conducted consistent with the recommendations in the Filterra maintenance manual provided by Contech Engineered Solutions.

^{6.} In the area governed by the Los Angeles Region Phase I stormwater permit, conventional biofilters must be sized to treat 1.5X the SWQDV. This results in an average annual capture rate of 93%. Filterra systems sized using this tool will also treat at least 93% of the average annual runoff volume.





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Phone: 949-217-4663

	Phone: 94:	9-217-4663	
Contact Information		Project Information	
Engineer of Record Name	Robert Dizon	Project Name	Condor
Engineer of Record Company Name	D&D Engineering, Inc.	Project Location	Inglewood, CA
Engineer of Record Office Zip Code	90301	Catchment Name	DA-10
Drainage Area Inputs			
Drainage Area		46835	ft ⁻
Runoff coefficient		0.9	-
Time of concentration		15	min
Long term reliable infiltration rate	Long term reliable infiltration rate		in/hr
85th percentile, 24-hour depth (see hype	rlink below)	1.05	in
LA County Rainfall Depth Analysis		Economic Control Contr	
Filterra Configuration (Select from Drop-Down)		Internal Bypass Curb	
Refer to "Filterra Configurations" tab for	descriptions and standard detai	ls for download.	
Constants			
LAX Airport 85th Percentile, 24-hour dep	th (for reference only)	1.02	in
Filterra hydraulic loading capacity		1.45	gpm/ft ²
<u>Outputs</u>			
Stormwater Quality Design Volume		3,688	ft ³
Design Rainfall Intensity for Equivalent Lo	ong Term Capture	0.359	in/hr
Site Scaling Factor		1.03	-
Stormwater Quality Design Flow Rate		0.36	cfs
Design Alternatives Available	Design Alternatives Available		
Design Recommendations			
Primary Recommendation - Stand Alo	ne Filterra		
Adjusted Filterra Design Intensity		0.514	in/hr
Stormwater Quality Design Flow Rate		0.52	cfs
Required Filterra Area		160	ft ²
Filterra Model ID		See Note	
Note: Drainage area is too large for single Filterra :	system. Consider a different Filterra co	nfiguration, utilizing multiple structures, or utilizing	Filterra Bioscape. Contact Contech
for more info.			
Alternative Recommendation - Filterro	a + Infiltration Storage		
Required Filterra Area		112	ft ²
Filterra Model ID		See Note	
ChamberMaxx volume		494	ft ³
ChamberMaxx count		7	chambers
1	system. Consider a different Filterra co	nfiguration, utilizing multiple structures, or utilizing	Fiiterra Bioscape. Contact Contech
for more info.			

- 1. Filterra systems must be designed and sized following the methodology in Section 4 of the August 2015 report prepared by Geosyntec Consultants, entitled "Filterra Equivalency Analysis and Design Criteria" which is the basis for this design tool.
- 2. Filterra systems use an engineered biofiltration media. Filterra systems, including the engineered biofiltration media, must be provided by the manufacturer. No substitution of materials/media is allowed.
- 3. Filterra is only applicable as an alternative on-site biofiltration design in situations where a project applicant has demonstrated that it is technically infeasible to retain 100 percent of the SWQDv onsite.
- 4. Hydromodification requirements of Section VI.D.7.c.iv of the Los Angeles County MS4 Permit must be considered separately regardless of what type of biofiltration is used.
- 5. Operation and maintenance of Filterra systems must be conducted consistent with the recommendations in the Filterra maintenance manual provided by Contech Engineered Solutions.
- 6. In the area governed by the Los Angeles Region Phase I stormwater permit, conventional biofilters must be sized to treat 1.5X the SWQDV. This results in an average annual capture rate of 93%. Filterra systems sized using this tool will also treat at least 93% of the average annual runoff volume.